

# Appendix to “Force-induced desorption and unzipping of semiflexible polymers”

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In this Appendix I present details on the theory of thermal desorption of semiflexible polymers and on the desorption kinetics.

*Thermal desorption.* In the absence of a desorbing force ( $f_d = 0$ ), a semiflexible polymer can undergo thermal desorption, which we want to describe using a model connecting length scales below and above the persistence length  $L_p \equiv 2\kappa/T$  ( $k_B \equiv 1$ ). At the desorption transition the correlation length  $\xi_{\parallel}$ , which gives the typical length of thermally desorbed segments, diverges. If the length of desorbed segments is comparable or smaller than  $L_p$ , i.e., for  $\xi_{\parallel} < L_p$  we apply the theory for the adsorption of a weakly bent *semiflexible* polymer [1], whereas we apply standard results for the adsorption of *flexible* Gaussian polymers [2] in combination with an effective or renormalized adsorption potential for  $\xi_{\parallel} > L_p$ . Using this approach we obtain a result for the critical potential strength  $W_c$  for thermal desorption and for the free energy of adsorption  $f_W$  which describes the full crossover from the semiflexible to the flexible regime.

On length scales comparable or smaller than  $L_p$ , the thermally fluctuating semiflexible polymer is only weakly bent and stays oriented, say along the  $x$ -axis. The desorption transition can then be described by the one-dimensional distance  $z(x)$  of polymer segments from the adsorbing surface  $z = 0$ , where  $0 < x < L$  and  $L < L_c$  is the projected polymer length. Bending and adhesion energy of the weakly bent semiflexible polymer give a Hamiltonian

$$\mathcal{H}_{\text{SF}} = \int_0^L dx \left[ \frac{\kappa}{2} (\partial_x^2 z)^2 + V(z(x)) \right]. \quad (1)$$

We consider generic square well adsorption potentials of range  $\ell$ , as they arise from van der Waals forces, screened electrostatic interactions, and crosslinking molecules. In these cases, the potential range  $\ell$  is comparable to the polymer thickness, the Debye-Hückel screening length, and the size of the linker molecule, respectively. For simplicity we neglect a possible orientation dependence in crosslinker-mediated adhesion [1] and consider adhesive square well potentials

$$V(z) = \begin{cases} W & \text{for } z < \ell \\ 0 & \text{for } z > \ell \end{cases} \quad (2)$$

where  $W < 0$  is the bare adhesion strength and  $V(z) = \infty$  for  $z < 0$  due to the hard wall.

The desorption transition for this Hamiltonian has been studied by transfer matrix techniques in Ref. [1]. The critical potential strength for desorption is

$$W_{c,\text{SF}} = -\frac{\sqrt{3\pi}}{2} \frac{T}{\ell^{2/3} L_p^{1/3}}, \quad (3)$$

The transfer matrix treatment shows that the free energy difference between adsorbed and free state vanishes as

$$f_{W,\text{SF}} \approx W_{c,\text{SF}} |w_{\text{SF}}| / \ln |w_{\text{SF}}|^{-1} \quad (4)$$

where  $w_{\text{SF}} \equiv (W - W_{c,\text{SF}})/W_{c,\text{SF}}$  is the reduced potential strength. Therefore, the correlation length  $\xi_{\parallel} = T/|f_{W,\text{SF}}| \propto |w_{\text{SF}}|^{-\nu}$  diverges with an exponent  $\nu = 1 + \log$ .

The weak bending approximation is valid as long as tangent angles are small, i.e.,  $\langle \phi^2 \rangle \sim \langle (\partial_x z)^2 \rangle \sim \xi_{\parallel}/L_p \lesssim 1$ , which is equivalent to the condition  $\xi_{\parallel} \lesssim L_p$  mentioned above. This condition is fulfilled for  $|W - W_{c,\text{SF}}| \gtrsim T/L_p$ , i.e., outside a window of adhesion strengths of width  $T/L_p$  around the critical value  $W_{c,\text{SF}}$ .

For  $\xi_{\parallel} \gg L_p$ , i.e., for  $|W - W_{c,\text{SF}}| \ll T/L_p$ , the semiflexible polymer is described as effectively flexible Gaussian polymer with  $N = L_c/L_p$  essentially uncorrelated Kuhn segments of length  $b = L_p$ . Each adsorbed Kuhn segment of length  $b \equiv L_p$  is weakly bent and performs small scale fluctuations governed by the Hamiltonian  $\mathcal{H}_{\text{SF}}$ , which gives rise to an *effective* adsorption potential  $V_{\text{eff}}(z)$ , which contains entropic contributions from small scale fluctuations.  $V_{\text{eff}}(z)$  is also short-ranged and can be assumed to have the same square well form (2) as the bare potential but with the effective binding energy

$$W_{\text{eff}} = f_{W,\text{SF}} \sim W - W_{c,\text{SF}} \quad (5)$$

given by the free energy of adsorption of each semiflexible Kuhn segment and a potential width  $\ell_{\text{eff}} = L_p$  set by the thermal fluctuations  $\langle z^2 \rangle \sim b^3/L_p = L_p^2$  of each Kuhn segment. In (5) we neglected the small logarithmic correction in (4).

The critical properties of the actual desorption transition are obtained in the limit of large  $\xi_{\parallel}$  and, thus, given by the critical behaviour of the effective flexible polymer model. The Kuhn segment length  $b = L_p$  and the effective adsorption potential  $V_{\text{eff}}(z)$  contain all effects from the bending rigidity. The standard transfer matrix approach for Gaussian polymers [2] shows that the critical effective potential for thermal desorption is

$W_{\text{eff},c} = -\frac{\pi^2}{24} \frac{T}{L_p}$ . Using (5) this is equivalent to a bare critical potential for desorption

$$\begin{aligned} W_c &\approx W_{c,\text{SF}} \left[ 1 - \frac{\pi^2}{24} (\ell/L_p)^{2/3} \right] \\ &\approx -\frac{\sqrt{3\pi}}{2} \frac{T}{\ell^{2/3} L_p^{1/3}} \left[ 1 - \frac{\pi^2}{24} (\ell/L_p)^{2/3} \right]. \end{aligned} \quad (6)$$

Because  $W_c < W_{c,\text{SF}}$ , the polymer indeed desorbs in the flexible regime that describes the large scale behavior. The free energy of adsorption in the effective flexible polymer model is given by

$$f_W \approx 3W_{\text{eff}}^2 L_p / T \sim 3(W - W_{c,\text{SF}})^2 L_p / 2T \quad (7)$$

The correlation length  $\xi_{\parallel} = T/|f_W| \propto |w|^{-\nu}$ , where  $w \equiv (W - W_c)/W_c$ , diverges with an exponent  $\nu = 2$ .

The critical properties of the desorption transition at  $W = W_c$  are described by the *flexible* polymer model, i.e., thermal desorption is of second order with  $\nu = 2$ . On the other hand, the transition point  $W_c \sim W_{c,\text{SF}}$  and apparent critical properties in the entire region  $|W - W_c| \gtrsim T/L_p$  are governed by the *semiflexible* Hamiltonian  $\mathcal{H}_{\text{SF}}$  with  $\nu = 1 + \log$ .

For  $\xi_{\parallel} < L_p$  or  $|W - W_c| \gtrsim T/L_p$  the free energy of adsorption  $f_W = f_{W,\text{SF}}$  is given by the free energy of adsorption (4) of a semiflexible polymer. For  $\xi_{\parallel} \gg L_p$  or  $|W - W_c| \ll T/L_p$ , on the other hand, the free energy of adsorption is given by the result (7). Neglecting the small logarithmic corrections in the result (4), we obtain a consistent crossover scenario for the free energy of adsorption, which connecting length scales below and above  $L_p$ :

$$|f_W| \approx \begin{cases} 3(W - W_c)^2 L_p / 2T & \text{for } |W - W_c| \ll T/L_p \\ |f_{W,\text{SF}}| \sim |W - W_c| & \text{for } |W - W_c| \gtrsim T/L_p \end{cases} \quad (8)$$

The semiflexible regime is characterized by  $|W - W_c| \gtrsim T/L_p$ , which is equivalent to  $|f_W| \gtrsim T/L_p$  or  $\xi_{\parallel} \lesssim L_p$ . The flexible regime is characterized by  $|W - W_c| \ll T/L_p$ , which is equivalent to  $|f_W| \ll T/L_p$  or  $\xi_{\parallel} \gg L_p$ .

*Constrained free energy for thermal desorption of a semiflexible polymer.* The thermal desorption of a weakly bent semiflexible polymer in the regime  $|f_W| = T\xi_{\parallel} \gtrsim T/L_p$  as described by the Hamiltonian  $\mathcal{H}_{\text{SF}}$  has been studied by transfer matrix techniques in Ref. [1]. This approach also allows to calculate the restricted partition sum  $Z(h)$  over all polymer configurations with a given height  $h$  of the end point. In Ref. [1], the scaling form

$$Z(h) = (h/L_p)^{\theta/2+1/3} \Omega(L_p^{1/2} h / \xi_{\parallel}^{3/2}) e^{L/\xi_{\parallel}} \quad (9)$$

for the restricted partition sum with a critical exponent  $\theta = -5/3$  characterizing the segment distribution close to the wall has been derived, together with an explicit result for the shape function

$$\Omega(y) \propto \int_0^{\infty} d\alpha \alpha^{-1/2} e^{-\alpha - 2y/3\alpha} = \sqrt{\pi} e^{-(8y/3)^{1/2}}. \quad (10)$$

Using (10) in (9) we obtain the constrained free energy

$$\begin{aligned} \Delta F(h) &= -T \ln[Z(h)/Z(0)] \\ &= -\frac{T}{2} \ln \left( \frac{h}{L_p} \right) + \frac{2^{7/4}}{3^{1/2}} h^{1/2} \kappa^{1/4} |f_W|^{3/4} \end{aligned} \quad (11)$$

of a weakly bent semiflexible polymer.

*Desorption kinetics.* Here we give more details on the analysis of the thermally activated desorption kinetics in the semiflexible regime  $|f_W| \gtrsim T/L_p$ . The analysis is based on the time-dependent probability  $P(t)$  of finding the polymer still adsorbed at time  $t$ . With the Arrhenius-type desorption rate  $k_d \sim \tau^{-1} e^{-f_0/f_d}$ , where  $f_0 \equiv L_p^{1/2} |f_W|^{3/2} / T^{1/2}$ , the kinetics of desorption is governed by the differential equation

$$dP/dt = -k_d P \quad (12)$$

for the probability  $P(t)$ . Analogous formulations have been used to describe the rupture of molecular bonds, see [3], where  $P(t)$  corresponds to the probability of finding the bond intact at time  $t$ .

For a time-constant force  $f_d > f_{d,c}$ , eq. (12) simply gives  $P(t) = e^{-k_d t}$ . Also for a time-ramped force  $f_d(t) = r_d t$ , which increases from the critical force with a constant and slow loading rate  $r_d \ll f_0/\tau$  the desorption kinetics is dominated by thermal activation, and we find  $P(t) = \exp(-\int_0^t d\tilde{t} k_d(\tilde{t}))$ . The most probable desorption time  $t^*$  maximizes the probability  $P(t)k_d(t)$  of desorption at time  $t$ , i.e.,  $\frac{d}{dt}|_{t^*} (P(t)k_d(t)) = 0$ . Using (12) this condition finally leads to the self-consistent equation

$$\tau e^{f_0/r_d t^*} = r_d t^{*2} / f_0 \quad (13)$$

for  $t^*$ . The desorption process is thermally activated for  $r_d < f_0/t^*$ . In this regime we find

$$t^* \sim (f_0/r_d) / \ln(f_0/r_d \tau) \quad (14)$$

and the condition for thermally activated behavior is indeed fulfilled for a slow loading rate  $r_d \ll f_0/\tau$ . In the opposite limit of fast loading rates  $r_d \gg f_0/\tau$ , the barrier becomes smaller than  $T$  before the polymer starts to desorb and the process is no longer thermally activated.

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